Advisory Note

Techniques and approaches contained in this handbook are not all-inclusive, nor universally applicable. Designing stream restorations requires appropriate training and experience, especially to identify conditions where various approaches, tools, and techniques are most applicable, as well as their limitations for design. Note also that product names are included only to show type and availability and do not constitute endorsement for their specific use.
Technical Supplement 14F

Pile Foundations

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Pile Foundations

Purpose

Piles are used to transfer foundation forces through relatively weak soil to stronger strata to minimize settlement. The most likely applications for pile foundations in stream restoration and stabilization projects are as support for bank stabilization structures (retaining wall) and anchors for large woody material (LWM). Piles may be used to support ancillary structures such as culverts, structural channels, bridges, and pumping stations. This technical supplement addresses the analyses required to design pile foundations.

Introduction

Foundation structures may be classified into two categories: shallow and deep. There is no specific rule that defines when a particular structure is considered to be shallow or deep. In general, shallow structures are constructed fairly close to ground surface and are usually constructed upwards from the bottom surface of an excavation.

Traditionally, deep foundations refer to piles that are driven into the ground. However, piles are sometimes set into holes that are prebored or drilled into the ground. A hole bored into the ground and filled with concrete is called a drilled shaft. Usually, reinforcing steel is placed into the drilled hole just prior to placement of the concrete. Other terms for drilled shafts are: drilled piers, drilled caissons, cast-in-place piles, cast-in-drilled-hole piles, and augered piles. Another type of drilled shaft foundation is an auger-cast pile.

Piles are typically installed using specialized pile driving equipment. The motive force that drives the pile into the ground is applied by a pile driving hammer, which is attached to the top of a pile. A crane is used to support the pile driving equipment and handle the individual piles.

Bearing capacity

The allowable bearing or axial capacity of a driven pile may be determined from the following equation:

\[
Q_{\text{Allowable}} = \frac{Q_{\text{total}}}{\text{factor of safety}} \quad \text{(eq. TS14F–1)}
\]

\[
Q_{\text{total}} = Q_{\text{point}} + Q_{\text{friction}} - W_{\text{pile}} \quad \text{(eq. TS14F–2)}
\]

where:

- \( Q_{\text{total}} \) = ultimate capacity of pile
- \( Q_{\text{point}} \) = end-bearing capacity of pile
- \( Q_{\text{friction}} \) = capacity due to friction along length of pile
- \( W_{\text{pile}} \) = weight of pile
- factor of safety = 3.0
For a cohesionless soil, the following formulas may be used to determine values (table TS14F–1) for the components of the bearing capacity equation:

\[
Q_{\text{point}} = \gamma' D N' A_{\text{point}}
\]

(eq. TS14F–3)

where:

- \( \gamma' \) = effective unit weight of soil
- \( D \) = embedded depth of pile
- \( A_{\text{point}} \) = area of pile tip

\[
N' = e^{x \tan \phi'} \tan^2 \left( 45^\circ + \frac{\phi'}{2} \right)
\]

(eq. TS14F–3a)

where:

- \( \phi' \) = \( \tan^{-1} (0.67 \tan \phi) \)
- \( \phi \) = angle of internal friction of soil

\[
Q_{\text{friction}} = \tau_{\text{average}} \sum_{\sigma} K_{\text{shape}} D
\]

(eq. TS14F–4)

where:

\[
\tau_{\text{average}} = \gamma' z K_o \tan \phi'
\]

(eq. TS14F–4a)

where:

- \( \gamma' \) = effective unit weight of soil
- \( z \) = depth (along pile) at point of analysis
- \( K \) = ratio of lateral to vertical soil stress on pile
  - \( K_o = 0.7 \) for piles loaded in compression
  - \( K_o = 0.5 \) for piles loaded in tension
- \( \phi' \) = \( \tan^{-1} (0.67 \tan \phi) \)
- \( \phi \) = soil angle of internal friction
- \( \Sigma \) = perimeter of pile
- \( K_{\text{shape}} \) = pile shape factor
  - \( K_{\text{shape}} = 1.000 \) for round perimeter
  - \( K_{\text{shape}} = 0.785 \) for square perimeter
  - \( K_{\text{shape}} = 0.95 \) for octagon perimeter
  - \( K_{\text{shape}} = 0.84 \) for hexagon perimeter
  - \( K_{\text{shape}} = 0.60 \) for triangular perimeter
- \( D \) = depth of pile

I-beam piles are considered to have a square perimeter with side lengths equivalent to their respective depth and width dimensions.

**Table TS14F–1** Prescriptive values for cohesionless soils

<table>
<thead>
<tr>
<th>Soil type</th>
<th>Angle of internal friction (°)</th>
<th>Angle of friction between soil and pile (°)</th>
<th>Bearing capacity coefficient ( N_q )</th>
<th>Maximum allowable capacity, ( Q )</th>
</tr>
</thead>
<tbody>
<tr>
<td>Clean sand</td>
<td>35</td>
<td>30</td>
<td>11</td>
<td>1.00 (100)</td>
</tr>
<tr>
<td>Silty sand</td>
<td>30</td>
<td>25</td>
<td>7</td>
<td>0.85 (50)</td>
</tr>
<tr>
<td>Sandy silt</td>
<td>25</td>
<td>20</td>
<td>5</td>
<td>0.70 (30)</td>
</tr>
<tr>
<td>Silt</td>
<td>20</td>
<td>15</td>
<td>4</td>
<td>0.50 (20)</td>
</tr>
</tbody>
</table>
For a cohesive soil, the following formulas may be used to determine values (table TS14F–2) for the components of the bearing capacity equation cited above.

\[ Q_{\text{point}} = A_{\text{point}} (7.4 + \gamma D) \quad \text{(eq. TS14F–5)} \]

where:
- \( A_{\text{point}} \) = area of pile tip
- \( c \) = shear strength of cohesive soil at pile tip depth
- \( \gamma \) = effective unit weight of soil
- \( D \) = depth of pile

\[ Q_{\text{friction}} = c'_{\text{average}} \sum_{\theta} K_{\text{shape}} D \quad \text{(eq. TS14F–6)} \]

where:
- \( c'_{\text{average}} \) = average effective shear stress of soil, along with a given length, or segment of the pile
- \( \sum_{\theta} \) = perimeter of pile
- \( K_{\text{shape}} \) = pile shape factor
- \( K_{\text{shape}} = 1.000 \) for round perimeter
- \( K_{\text{shape}} = 0.785 \) for square perimeter
- \( D \) = depth of pile or length of pile segment

### Table TS14F–2 Prescriptive values for cohesive soils

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<th>Clay</th>
<th>Shear strength</th>
</tr>
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<tr>
<td>Normally consolidated</td>
<td>( c_s = 0.5\gamma'z(1-K_o) )</td>
</tr>
<tr>
<td>Underconsolidated</td>
<td>( c_z = 0.125\gamma'z(1-K_o) )</td>
</tr>
<tr>
<td>Overconsolidated by erosion</td>
<td>( c_z = 600 \text{ lb/ft}^2 + 0.5\gamma'z(1-K_o) )</td>
</tr>
<tr>
<td>Overconsolidated by desiccation</td>
<td>( c_z = 2,000 \text{ lb/ft}^2 ) \text{ for } z = 0 \text{ ft to 20 ft}</td>
</tr>
<tr>
<td></td>
<td>( c_z = 1,200 \text{ lb/ft}^2 ) \text{ for } z = 20 \text{ ft to 60 ft}</td>
</tr>
<tr>
<td></td>
<td>( c_z = 3,000 \text{ lb/ft}^2 ) \text{ for } z = 60 \text{ ft to 160 ft}</td>
</tr>
</tbody>
</table>

For highly fissured clays, use the following:

\( c' = 0 \)

\( \phi' = 5' \text{ to } 10' \) and

\( t'_{\text{average}} = \gamma' z K_o \tan \phi' \)

Notes:
- For piles loaded in axial compression, \( K_o = 0.7 \)
- For piles loaded in axial tension, \( K_o = 0.5 \)
- Effective shear strength, \( c' = 0.67c \)
- \( Z = \) depth along pile from ground surface (ft) \( Z = 0 \) at ground surface
Lateral load capacity

An approximate lateral capacity of a short, rigid pile driven into a cohesive soil can be determined from the following equation (figs. TS14F–1 and TS14F–2):

\[ P_{\text{Allowable}} = \frac{P_{\text{Ultimate}}}{\text{factor of safety}} \quad \text{(eq. TS14F–7)} \]

where:
- \( P_{\text{Allowable}} \) = allowable lateral load applied to exposed portion of pile
- factor of safety = 3

\[ P_{\text{Ultimate}} = \sigma B \left( \sqrt{\frac{4}{2} (D + H)^2 + D^2} \right) - 2 \left( \frac{D}{2} + H \right) \quad \text{(eq. TS14F–8)} \]

where:
- \( \sigma \) = allowable soil stress, \( \sigma = 9c \)
- \( B \) = width or diameter of pile
- \( D \) = depth of pile embedment
- \( H \) = height of pile (above ground) to centroid of applied load

If a design load is known, the required depth of embedment may be determined from the following equation:

\[ D = \frac{P_{\text{Ultimate}} \gamma' B K_p D^2}{2(H + D)} \quad \text{(eq. TS14F–12)} \]

where:
- \( \gamma' \) = effective unit weight of soil
- \( B \) = width or diameter of pile
- \( K_p \) = passive pressure coefficient
- \( \phi \) = soil angle of internal friction
- \( D \) = embedded depth of pile

\[ K_p = \tan^2 \left( 45' + \frac{\phi}{2} \right) \quad \text{(eq. TS14F–13)} \]

If a design load is known, the required depth of embedment may be determined from the following equation.

\[ D = \frac{\sqrt{2P_{\text{Ultimate}}}}{\gamma' B K_p (H + D)} \quad \text{(eq. TS14F–14)} \]

This equation is solved iteratively until both values for \( D \) are equivalent.

For most stream restoration and stabilization applications, a driven pile may be considered to be rigid when:

\[ \frac{H}{B} \leq 12 \quad \text{(eq. TS14F–10)} \]

An approximate allowable lateral load for a short, rigid pile driven into a cohesionless soil may be determined using the following equation (figs. TS14F–3 and TS14F–4).

\[ P_{\text{Allowable}} = \frac{P_{\text{Ultimate}}}{\text{factor of safety}} \quad \text{(eq. TS14F–11)} \]

where:
- \( P_{\text{Allowable}} \) = allowable lateral load applied to exposed portion of pile
- factor of safety = 3
Figure TS14F–1  Schematic showing applied lateral force and assumed soil reactions for single rigid pile driven into a cohesive soil. Concentrated load applied at top of pile

Figure TS14F–2  Schematic showing applied lateral force and assumed soil reactions for a single rigid pile driven into a cohesive soil. Uniformly decreasing load applied
**Figure TS14F–3**  Schematic showing applied lateral force and assumed soil reactions for single rigid pile driven into a cohesive soil. Concentrated load applied at top of pile

\[ \sigma_D = 3\gamma' D_K_p \]

\[ \sigma_Z = 3\gamma' Z_K_p \]

**Figure TS14F–4**  Schematic showing applied lateral force and assumed soil reactions for single rigid pile driven into a cohesive soil. Uniformly decreasing load applied as shown

\[ \sigma_D = 3\gamma' D_K_p \]

\[ \sigma_Z = 3\gamma' Z_K_p \]